

UDK 669.15-194.57:620.179.16:539.43

I. A. VAKULENKO^{1*}, YU. L. NADEZH DIN², V. A. SOKYRKO³, XU XIAO HAI⁴^{1*}Dep. «Technology of Materials», Dnipropetrovsk National University of Railway Transport named after Academician V. Lazaryan, Lazaryan St., 2, Dnipropetrovsk, Ukraine, 49010, tel. +38 (056) 373 15 56, e-mail dnuzt_textmat@ukr.net, ORCID 0000-0002-7353-1916²Dep. «Technology of Materials», Dnipropetrovsk National University of Railway Transport named after Academician V. Lazaryan, Lazaryan St., 2, Dnipropetrovsk, Ukraine, 49010, tel. +38 (056) 373 15 56, e-mail 7435892@gmail.com, ORCID 0000-0003-1805-4616³DS Ltd, Scientific-industrial company, B. Morskay St., 63, Mykolaiv, Ukraine, 54001, tel. +38 (0512) 35 44 83, e-mail ds@mksat.net, ORCID 0000-0002-0338-5976⁴China machinery investment group Ltd, Anli Road, 60, Chaoyang District, Beijing, China, 100101, tel. 86 106 482 7530, e-mail xxhai2004@163.com, ORCID 0000-0001-7051-6254SPEED DEPENDENCE OF ACOUSTIC VIBRATION PROPAGATION
FROM THE FERRITIC GRAIN SIZE IN LOW-CARBON STEEL

Purpose. It is determining the nature of the ferrite grain size influence of low-carbon alloy steel on the speed propagation of acoustic vibrations. **Methodology.** The material for the research served a steel sheet of thickness 1.4 mm. Steel type H18T1 had a content of chemical elements within grade composition: 0, 12 % C, 17, 5 % Cr, 1 % Mn, 1, 1 % Ni, 0, 85 % Si, 0, 9 % Ti. The specified steel belongs to the semiferitic class of the accepted classification. The structural state of the metal for the study was obtained by cold plastic deformation by rolling at a reduction in the size range of 20-30 % and subsequent recrystallization annealing at 740 – 750 ° C. Different degrees of cold plastic deformation was obtained by pre-selection of the initial strip thickness so that after a desired amount of rolling reduction receives the same final thickness. The microstructure was observed under a light microscope, the ferrite grain size was determined using a quantitative metallographic technique. The using of X-ray structural analysis techniques allowed determining the level of second-order distortion of the crystal latitude of the ferrite. The speed propagation of acoustic vibrations was measured using a special device such as an ISP-12 with a working frequency of pulses 1.024 kHz. As the characteristic of strength used the hardness was evaluated by the Brinell's method. **Findings.** With increasing of ferrite grain size the hardness of the steel is reduced. In the case of constant structural state of metal, reducing the size of the ferrite grains is accompanied by a natural increasing of the phase distortion. The dependence of the speed propagation of acoustic vibrations up and down the rolling direction of the ferrite grain size remained unchanged and reports directly proportional correlation. **Originality.** On the basis of studies to determine the direct impact of the proportional nature of the ferrite grain size on the rate of propagation of sound vibrations in the low-carbon alloy steel. The directly proportional nature of influence of ferrite grain size on the speed propagation of acoustic vibrations in low-carbon alloy steel on the basis of the conducted researches is defined. The paper is shown that at increasing in the size of the recrystallized ferrite grain the degree of influence the texture from the previous cold plastic deformation by rolling increases. **Practical value.** The received results on nature determination of influence of ferrite grain size on the speed propagation of acoustic vibrations can be the useful by development of techniques of non-destructive testing of metal materials quality. The special value the specified technique of measurement acquires in the conditions of line production of metal constructions.

Key words: hardness index; grain size; ferrite; phase distortion; speed propagation of acoustic vibration

Introduction

In modern conditions of the industry development, the intensification of production is impossible without the development of automated control systems of technological processes [1, 10].

Based on this, the requirements are quite reasonably increasing on the accuracy and speed evaluation of the metallic material properties [2], or the degree defectiveness during the using of the product [9], in

which is necessary for the timely adjustment of parameters of technological processes. These automated systems in most cases based on the use of non-destructive methods for determining the properties of metals and alloys [6]. The numerical technique for modeling the propagation of elastic waves in materials received the application [12], methods for measuring physical properties of metallic materials, which include methods of acoustic measurement [13, 14], acoustic emission, magnetic [11], and other properties.

The state of the question

To some of the known acoustic methods for assessing the properties of metals and alloys include the method of measuring the speed propagation of acoustic vibration (V) [8]. These specifications are structure-sensitive value to the internal structure of the metallic material. By the results of research show the sensitivity of the speed propagation of acoustic vibration to changes in the strength characteristics [13], the structural state of metal [14]. On the other hand, for example, carbon steel the same level of strength can be achieved by varying the ratio of morphology and dispersion of particles of the minor phase, the grain size of the metal matrix, the presence of substructure [4] and others. Based on this, rather complex overall impact of structural components in multiphase alloys magnitude to speed propagation of acoustic vibration [8] indicates the necessity for continued research. Making a detailed analysis of the nature of the expected dependency rate speed propagation of acoustic vibration from the characteristics of the internal structure of the metal may be useful for the development of non-destructive testing methods, particularly in the difficult conditions of loading system “wheel – rail” of railway transport [7].

Purpose

It is determining the nature of the ferrite grain size influence of low-carbon alloy steel on the speed propagation of acoustic vibrations.

Methodology

The material for the research served a steel sheet of thickness 1.4 mm. Steel type H18T1 had a content of chemical elements within grade composition: 0, 12 % C, 17, 5 % Cr, 1 % Mn, 1, 1 % Ni, 0, 85 % Si, 0, 9 % Ti. The specified steel belongs to the semiferritic class on the accepted classification.

The specified steel belongs to the semiferritic class on the accepted classification. The structural state of the metal for the study was obtained by cold plastic deformation by rolling at a reduction in the size range of 20-30 % and subsequent recrystallization annealing at 740 – 750 ° C. Different degrees of cold plastic deformation was obtained by pre-selection of the initial strip thickness so that after a desired amount of rolling reduction receives

the same final thickness.

The microstructure was observed under a light microscope, the ferrite grain size was determined using a quantitative metallographic technique. [3]. In order to understand the mechanism of ferrite grain size influence propagation of acoustic vibration in the metal determined the parameters of its fine crystal structure. The using of X-ray structural analysis techniques [5] allowed determining the level of second-order distortion of the crystal latitude of the ferrite.

The speed propagation of acoustic vibrations was measured using a special device such as an ISP-12 with a working frequency of pulses 1.024 kHz [8]. As the characteristic of strength used the hardness was evaluated by the Brinell's method. [3].

Findings and discussion

During the cold plastic rolling deformation draft the increasing of shrinkage accompanied by a steady rising in the number of accumulated defects in the crystal structure. With further annealing at the expense of recrystallization processes is the formation of homogeneous microstructure of ferrite grain size structure (d), which are inversely proportional to the degree of plastic deformation [4].

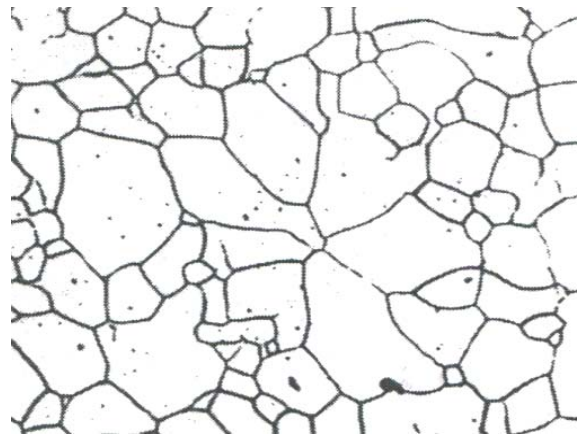


Fig.1. The microstructure of steel H18T1 after cold plastic flow by the rolling and annealing at a temperature of 750 °C. Magnification is 100.

The magnitude of the grain size varied in the range 43-65 μm . The typical microstructure of investigated steel is shown on Figure 1. Normal distribution of grains in size is a confirmation of the completion process of building recrystallization.

With increasing ferrite grain size the steel hard-

МАТЕРІАЛОЗНАВСТВО

ness, like most of the strength characteristics [4,15], decreases (Fig.2). The shown dependence is well obeys the equation of Hall-Petch type relation

$$HB = HB_0 + kd^{-\frac{1}{2}}, \quad (1)$$

where HB_0 – the steel hardness at the infinitely large ferrite grain size, k – the angular dependency ratio. From the analysis of the ratio (Fig.2) were determined constant of equation (1), which amounted to the value $HB_0 = 8 \frac{kg}{mm^2}$, and

$k \approx 45 \frac{kg}{mm^{1,5}}$. Comparative analysis of the obtained characteristics with known parameters for most steels shows that HB_0 in absolute values approaching the shear stress of the ferrite crystal lattice, whereas similar magnitude exceeds by more than an order of magnitude [4]. Elevated values k are likely due to different stress state of the metal. Thus, measuring the hardness under the indenter is formed volumetric stress state, whereas in most studies devoted to the analysis of diagrams of the Hall-Petch relation, the tests were carried out in the uniaxial stress state at tensile.

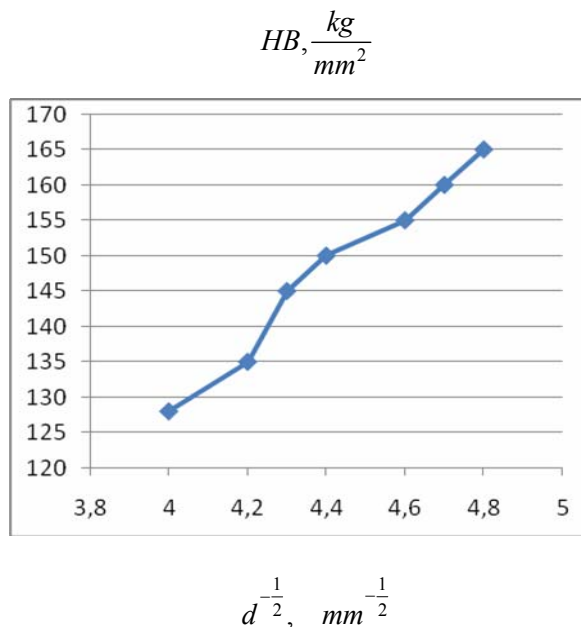


Fig.2. The dependence of the steel hardness from the ferrite grain size

Experimental studies determined that under certain conditions during heat treatment in the steel structure of the specified can remain the volume

fraction of residual austenite. To assess the possible influence of austenite on the steel hardness, determined the size of the lattice phase distortions for ferrite (μ). The comparative analysis of the magnitude μ of the steel hardness showed the existence of the directly-proportional ratio between them (Fig.3).

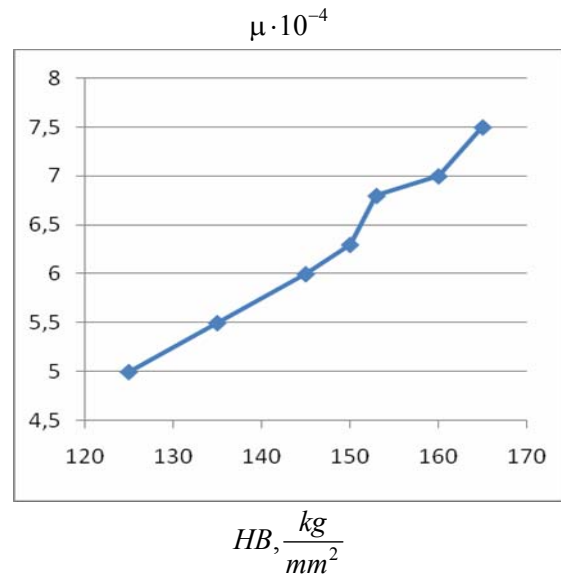


Fig.3. Mutual change of size μ and hardness.

Given the persistent structural state of metal ferrite grain size reduction is accompanied by quite natural growth of phase distortions. On this basis, it can be assume that for investigated the structural state of metal structure in the presence of austenitic phase does not lead to violations of the nature of ferrite grain size influence to the hardness and phase distortions.

The measurement of the velocity of propagation of sound vibrations in the metal from the grain size (Fig.4) showed the existence of influence the texture of cold plastic deformation by rolling. From the comparative analysis of the given correlations can determine that the dependence of the velocity of sound waves along (V_{vp}) and across (V_{pp}) in the direction from d remained unchanged and is accountable directly proportional to the ratio:

$$V = V_0 + \alpha d \quad (2)$$

where V_0 – the constant value and α – angular dependency ratio.

The influence of texture is reflected not only on the absolute values of the speed propagation of acous-

МАТЕРІАЛОЗНАВСТВО

tic vibrations, but also on the angular change of the dependency ratio.

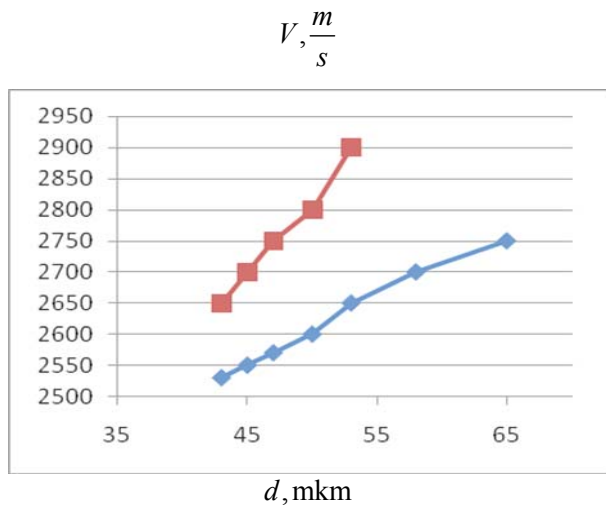


Fig.4. The dependence of the speed propagation acoustic vibrations from the grain size and the rolling direction: ■ - V_{vp} ♦ and ♦ - V_{pp}

Indeed, assessing the sensitivity of the speed propagation of acoustic vibrations in the steel prior to the change of grain size of ferrite in angular ratio $V = f(d)$ (fig. 4), it can be determine that the propagation of acoustic vibrations in the direction of rolling the magnitude of the sensitivity to changes d ($\alpha_1 = \frac{\Delta V_{vp}}{\Delta d}$) about in 2.5 times exceeds the similar characteristic to the rolling direction transversely ($\alpha_2 = \frac{\Delta V_{pp}}{\Delta d}$). The result is additional evidence of the impact of rolling texture on the value V of the tested metal. Although based on microstructural studies the influence after rolling recrystallization texture is difficult to define (fig.1). This is due by formed almost homogeneous microstructure of grain structure with no signs of forced orientation of the grains.

Thus, only a negligible impact from parts of the texture that is left after recrystallization, can be determined by measuring the speed propagation of acoustic vibrations. The analysis of experimental results confirmed the given situation that the influence of the remnants of the texture of cold rolling and subsequent annealing of increasing ferrite grain size is reflected in the change V to a greater extent.

On the basis of numerous experimental data it

is known that with increasing degree of cold plastic deformation occurs progressive increase in the number of centers of nucleation recrystallising grains. On this basis, it is quite clear that expectation of grain refinement of ferrite during annealing. On the other hand, by reducing the degree of cold plastic deformation significantly increases the likelihood of development of processes of polygonization subsequent heating [4]. For this reason, after an inadequate level of plastic deformation may develop processes of polygonization could greatly complicate the formation of germ recrystallising grains.

Thus, for the investigated steel the influence of texture from preliminary cold plastic deformation by rolling with the growth of the grain size must be manifested to a greater degree. As shown in the diagram it should be considered that the smaller degree of plastic deformation is subjected to the metal, the larger the grain size will be obtained after recrystallization annealing and will be more retained by the influence of cold rolling texture.

For the purpose of determining the absence of the influence of the rolling texture you need to use the dependencies V_{vp} and V_{pp} from the ferrite grain size (fig.4). Extrapolation of these dependencies in the area of small grain size to the point of intersection (when $V_{vp} \approx V_{pp}$) allows you to define the grain size, below which it should expect from the lack of influence of the rolling texture. The ferrite grain size has roughly equal 30-33mkm. Thus, to achieve almost complete absence of anisotropy properties after recrystallization annealing before cold-rolled is necessary to increase the degree of cogging. In this case, the processes of recrystallization will occur more fully and, as a consequence, there will be a more short-grain structure. To justify the submitted proposals were used constructed value correlation V_{vp} and V_{pp} from the steel hardness (fig.5). Implementation of extrapolation in areas of high hardness values just as it was done for according to the ferrite grain size (Fig.4), the moment when $V_{vp} \approx V_{pp}$ metal hardness value

should be at level $190-195 \frac{kg}{mm^2}$. If apply specified

hardness value deducted for experimental dependence HB from grain size (fig.2),

$$HB, \frac{kg}{mm^2}$$

МАТЕРІАЛОЗНАВСТВО

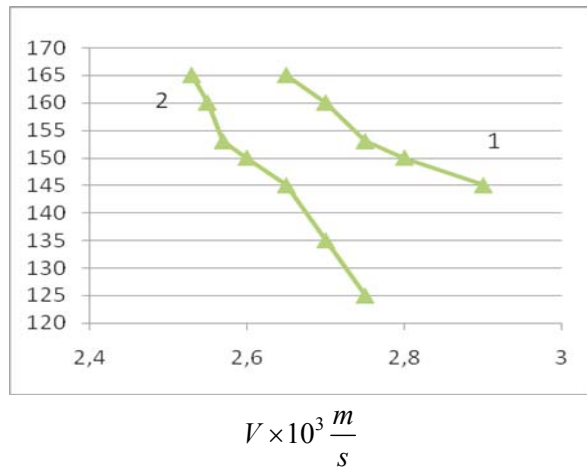


Fig.5. The correlation of the steel hardness and the propagation velocity of sound vibrations

(V_{vp-1} , V_{pp-2}).

get $d^{-\frac{1}{2}} \approx 5,8 \text{ mm}^{-\frac{1}{2}}$, that actually corresponds 30–33mkm. A similar grain size values obtained from the analysis of dependencies which are shown on figure 4.

Thus, in terms of the engineering industry applications of the measuring method of speed propagation of acoustic vibrations will allow to evaluate the degree of anisotropy of the properties of metallic materials, without costly testing the mechanical properties.

Originality and practical value

1. On the basis of research defined directly proportional to the impact of ferrite grain size on the propagation of acoustic vibrations in the low-carbon alloy steel.

2. It is shown that at increasing in size of recrystallising ferrite grain, the degree of texture influence from preliminary cold plastic deformation by rolling is grown up.

The results obtained by the determination of the ferrite grain size influence on the speed propagation of acoustic vibrations may be useful in the development of methods of nondestructive testing of metallic materials. The particular value is the specified method of measurement of gains in the ongoing manufacture of metal structures.

Conclusions

1. Analysis of the hardness dependence of steel from the ferrite grain size showed that the hardness

component, which determines the state of a solid solution substantially equal to the shear stress of the crystal lattice of the ferrite.

2. The angular dependency ratio of steel hardness from the ferrite grain size is determined by the influence of the remnants of the rolling texture after annealing recrystallization.

3. Shredding ferrite grain lowers the effect textures of rolling low carbon alloy steel after recrystallization annealing.

LIST OF REFERENCE LINKS

1. Акустический аспект шероховатости рельсов и колес // Ж.-д. дороги мира. – 2010. – № 12. – С. 71–74.
2. Басов, Г. Г. Анализ систем неразрушающего контроля при изготовлении подвижного состава железных дорог / Г. Г. Басов, А. Н. Киреев // Локомотив – Информ. – 2010. – № 11. – С. 30–42.
3. Вакуленко, І. О. Структурний аналіз в матеріалознавстві / І. О. Вакуленко. – Дніпропетровськ : Маковецький, 2010. – 124 с.
4. Вакуленко, І. А. Морфология структуры и деформационное упрочнение стали / І. А. Вакуленко, В. І. Большаков. – Днепропетровск : Маковецкий, 2008. – 196 с.
5. Гинье, А. Рентгенография кристаллов. Теория и практика / А. Гинье. – Москва : Физматгиз, 1961. – 604 с.
6. Контроль осей колесных пар по методу компании ННА // Ж.-д. дороги мира. – 2010. – № 12. – С. 53–58.
7. Куліченко, А. Я. Оцінка якісних показників контактування поверхневих шарів трибологічної системи «колесо–рейка» / А. Я. Куліченко, М. О. Кузін, І. О. Вакуленко // Наука та прогрес трансп. Вісн. Дніпропетр. нац. ун-ту заліз. трансп. – 2013. – № 3 (45). – С. 44–52. doi: 10.15802/stp2013/14529.
8. Муравьев, В. В. Исследование процесса распада пересыщенного твердого раствора в алюминиевом сплаве Д16 / В. В. Муравьев, М. Р. Ноева, А. В. Шарко // Физика металлов и металловедение. – 1978. – Т. 46, Вып. 4. – С. 746–749.
9. A damage parameter for HCF and VHCF based on hysteretic damping / Y. Lage, H. Cachão, L. Reis [et al.] // Intern. J. of Fatigue. – 2014. – Vol. 62. – P. 2–9. doi: 10.1016/j.jif.2013.10.010.
10. Comprehensive Study of Thermal Transport and Coherent Acoustic-Phonon Wave Propagation in Thin Metal Film–Substrate by Applying Picosecond Laser Pump–Probe Method / M. Weigang, M.

МАТЕРІАЛОЗНАВСТВО

- Tingting, X. Zhang [et al.] // J. Phys. Chem. C. – 2015. – 119 (9). – P. 5152–5159. doi: 10.1021/jp512735k.
11. Langman, R. A. Estimation of Residual Stresses in Railway Wheels by Means of Stress Induced Magnetic Anisotropy / R. A. Langman, P. J. Mutton // NDT&E Intern. – 1993. – Vol. 26. – № 4. – P. 195–205. doi: 10.1016/0963-8695(93)90474-9.
 12. Numerical simulations of elastic wave propagation using graphical processing units – Comparative study of high-performance computing capabilities / P. Packo, T. Bielak, A. B. Spencer [et al.] // Computer Methods in Applied Mechanics and Engineering. – 2015. – Vol. 290. – P. 98–126. doi:10.1016/j.cma.2015.03.002.
 13. Ultra-sonic Resonance Method with EMAT for Stress Measurement in Thin Plates / H. Fukuoka, M. Higaro, T. Yamasaki [et al.] // Review of Progress in Quantitative Nondestructive Evaluation. – 1993. – № 12. – P. 2129–2136. doi:10.1007/978-1-4615-2848-7_273.
 14. Ultra-sonic Set-Up to Characterize Stress States in Rims of Railroad Wheels. / R. Herzer, H. Frotscher, K. Schillo [et al.] // Nondestructive Characterization of Materials VI. – 1994. – P. 699–706. doi: 10.1007/978-1-4615-2574-5_89.
 15. Vakulenko, I. A. The Influence Mechanism of Ferrite Grain Size on Strength Stress at the Fatigue of Low-carbon Steel / I. A. Vakulenko, S. V. Proydak // Наука та прогрес трансп. Вісн. Дніпропетр. нац. ун-ту залізн. трансп. – 2014. – № 1 (49). – С. 97–104. doi: 10.15802/stp-2014/22668.

І. О. ВАКУЛЕНКО^{1*}, Ю. Л. НАДЕЖДИН², В. А. СОКІРКО³, СЮ СЯ ХАЙ⁴

^{1*}Каф. «Технологія матеріалів», Дніпропетровський національний університет залізничного транспорту імені академіка В. Лазаряна, вул. Лазаряна, 2, Дніпропетровськ, Україна, 49010, тел. +38 (056) 373 15 56, ел. пошта dnuzt_texmat@ukr.net, ORCID 0000-0002-7353-1916

²Каф. «Технологія матеріалів», Дніпропетровський національний університет залізничного транспорту імені академіка В. Лазаряна, вул. Лазаряна, 2, Дніпропетровськ, Україна, 49010, тел. +38 (056) 373 15 56, ел. пошта 7435892@gmail.com, ORCID 0000-0003-1805-4616

³ДС ЛТД, Науково-виробнича компанія, вул. Велика Морська, 63, Миколаїв, Україна, 54001, тел. +38 (0512) 35 44 83, ел. пошта ds@mksat.net, ORCID 0000-0001-7051-6254

⁴Китайська машинобудівна інвестиційна група ЛТД, вул. Анли, 60, Пекін, Китайська народна республіка, 100101, тел. 86 10 64827530, ел. пошта xxhai2004@163.com, ORCID 0000-0002-0338-5976

ЗАЛЕЖНІСТЬ ШВИДКОСТІ РОЗПОВСЮДЖЕННЯ ЗВУКОВИХ КОЛИВАНЬ ВІД РОЗМІРУ ЗЕРНА ФЕРИТУ В НИЗЬКОВУГЛЕЦЕВІЙ СТАЛІ

Мета. Робота спрямована на визначення характеру впливу розміру зерна фериту низьковуглецевої легированої сталі на швидкість розповсюдження звукових коливань. **Методика.** Матеріалом для досліджень була обрана листовая сталь товщиною 1,4 мм. Сталь типу X18T1 мала вміст хімічних елементів у межах марочного складу: 0,12 % С, 17,5 % Cr, 1 % Mn, 1,1 % Ni, 0,85 % Si, 0,9 % Ti. За прийнятою класифікацією вказана сталь відноситься до напівферитного класу. Структурний стан металу для дослідження отримували в результаті холодної пластичної деформації прокату на величину обтискування в інтервалі 20–30 % і подальшого рекристалізаційного відпалу при температурах 740–750 °С. Різний ступінь холодної пластичної деформації отримували (завдяки попередньому підбору похідної товщини прокату) таким чином, щоб після прокатки на потрібну величину обтискування отримати однакову кінцеву товщину. Мікроструктуру досліджували під світловим мікроскопом, розмір зерна фериту визначали, використовуючи методики кількісної металографії. Застосування методик рентгенівського структурного аналізу дозволило визначити рівень викривлень кристалічної решітки другого роду фериту. Швидкість розповсюдження звукових коливань вимірювали спеціальним приладом типу ІСП-12 із робочою частотою проходження імпульсів 1,024 кГц. В якості характеристики міцності використовували твердість, яку оцінювали за методом Брінеля. **Результати.** При збільшенні розміру зерна фериту твердість сталі знижується. Приведена залежність підпорядковується рівнянню типу Хола-Петча. За умов незмінного структурного стану металу зменшення розміру зерна фериту супроводжується закономірним зростанням викривлень другого роду. Характер залежності швидкості розповсюдження звукових коливань уздовж й уперек напрямку прокатки від розміру зерна фериту залишається незмінним та підпорядковується прямо пропорційному співвідношенню. **Наукова новизна.** На основі проведених досліджень визначений прямо пропорційний характер впливу роз-

МАТЕРІАЛОЗНАВСТВО

міру зерна фериту на швидкість розповсюдження звукових коливань у низькоуглецевій легованій сталі. В роботі показано, що при зростанні розміру рекристалізованого зерна фериту ступінь впливу текстури від попередньої холодної пластичної деформації прокаткою збільшується. **Практична значимість.** Отримані результати з визначення характеру впливу розміру зерна фериту на швидкість розповсюдження звукових коливань можуть бути корисними при розробці методик неруйнівного контролю якості металевих матеріалів. Особливого значення вказана методика вимірювання набуває в умовах поточного виготовлення металевих конструкцій.

Ключові слова: твердість; розмір зерна; ферит; викривлення другого роду; швидкість розповсюдження звукових коливань

И. А. ВАКУЛЕНКО^{1*}, Ю. Л. НАДЕЖДИН², В. А. СОКИРКО³, СЮ СЯ ХАЙ⁴

^{1*}Каф. «Технология материалов», Днепропетровский национальный университет железнодорожного транспорта имени академика В. Лазаряна, ул. Лазаряна, 2, Днепропетровск, Украина, 49010, тел. +38 (056) 373 15 56, эл. почта dnuzt_texmat@ukr.net, ORCID 0000-0002-7353-1916

²Каф. «Технология материалов», Днепропетровский национальный университет железнодорожного транспорта имени академика В. Лазаряна, ул. Лазаряна, 2, Днепропетровск, Украина, 49010, тел. +38 (056) 373 15 56, эл. почта 7435892@gmail.com, ORCID 0000-0003-1805-4616

³ДС Лтд, Научно-производственная компания, ул. Большая Морская, 63, Николаев, Украина, 54001, тел. +38 (0512) 35 44 83, эл. почта ds@mksat.net, ORCID 0000-0001-7051-6254

⁴Китайская машиностроительная инвестиционная группа Лтд, ул. Анли, 60, Пекин, Китайская народная республика, 100101, тел. 86 10 64827530, эл. почта xxhai2004@163.com, ORCID 0000-0002-0338-5976

ЗАВИСИМОСТЬ СКОРОСТИ РАСПРОСТРАНЕНИЯ ЗВУКОВЫХ КОЛЕБАНИЙ ОТ РАЗМЕРА ЗЕРНА ФЕРРИТА В НИЗКОУГЛЕРОДИСТОЙ СТАЛИ

Цель. Работа направлена на определение характера влияния размера зерна феррита низкоуглеродистой легированной стали на скорость распространения звуковых колебаний. **Методика.** Материалом для исследований служила листовая сталь толщиной 1,4 мм. Сталь типа X18T1 имела содержание химических элементов в пределах марочного состава: 0,12 % C, 17,5 % Cr, 1 % Mn, 1,1 % Ni, 0,85 % Si, 0,9% Ti. Указанная сталь относится к полуферритному классу по принятой классификации. Структурное состояние металла для исследования получали в результате холодной пластической деформации прокаткой на величину обжатия в интервале 20—30 % и последующего рекристаллизационного отжига при температурах 740–750 °С. Различную степень холодной пластической деформации получали (благодаря предварительному подбору исходной толщины проката) таким образом, чтобы после прокатки на требуемую величину обжатия получалась одинаковая конечная толщина. Микроструктуру исследовали под световым микроскопом, размер зерна феррита определяли, используя методики количественной металлографии. Применение методик рентгеновского структурного анализа позволило определить уровень искажений второго рода кристаллической решетки феррита. Скорость распространения звуковых колебаний измеряли специальным прибором типа ИСП-12 с рабочей частотой прохождения импульсов 1,024 кГц. В качестве характеристики прочности использовали твердость, которую оценивали по методу Бринелля. **Результаты.** При увеличении размера зерна феррита твердость стали снижается. Приведенная зависимость подчиняется уравнению типа Холла-Петча. В случае неизменного структурного состояния металла уменьшение размера зерна феррита сопровождается закономерным ростом искажений второго рода. Характер зависимости скорости распространения звуковых колебаний вдоль и поперек направления прокатки от размера зерна феррита остается неизменным и подчиняется прямопропорциональному соотношению. **Научная новизна.** На основе проведенных исследований определен прямопропорциональный характер влияния размера зерна феррита на скорость распространения звуковых колебаний в низкоуглеродистой легированной стали. В работе показано, что при увеличении размера рекристаллизованного зерна феррита степень влияния текстуры от предыдущей холодной пластической деформации прокаткой возрастает. **Практическая значимость.** Полученные результаты по определению характера влияния размера зерна феррита на скорость распространения звуковых колебаний могут быть полезными при разработке методик неразрушающего контроля качества металлических материалов. Особенное значение указанная методика измерения приобретает в условиях поточного производства металлических конструкций.

Ключевые слова: твердость; размер зерна; феррит; искажение второго рода; скорость распространения звуковых колебаний

REFERENCES

1. Akusticheskiy aspekt sherokhovatosti relsov i koles [Acoustic aspect of rails and wheels roughness]. *Zheleznyye dorogi mira – Railways of the World*, 2010, no. 12, pp. 71-74.
2. Basov G.G., Kireyev A.N. Analiz sistem nerazrushayushchego kontrolya pri izgotovlenii podvizhnogo sostava zheleznykh dorog [Systems analysis of non-destructive control in the manufacture of railway rolling stock]. *Lokomotiv-Inform – Lokomotiv-Inform*, 2010, no. 11, pp. 30-42.
3. Vakulenko I.O. *Strukturnyi analiz v materialoznavstvi* [Structural analysis in materials science]. Dnipropetrovsk, Makovetskiy Publ., 2010. 124 p.
4. Vakulenko I.A., Bolshakov V.I. *Morfologiya struktury i deformatsionnoye uprochneniye stali* [The morphology of the structure and strain hardening of steel]. Dnepropetrovsk, Makovetskiy Publ., 2008. 196 p.
5. Gine A. *Rentgenografiya kristallov. Teoriya i praktika* [X-ray analysis of crystals. Theory and practice]. Moscow, Fizmatgiz Publ., 1961. 604 p.
6. Kontrol osey kolesnykh par po metodu kompanii NNA [The control axes of the wheel pairs by method of the company NNA]. *Zheleznyye dorogi mira – Railways of the World*, 2010, no. 12, pp. 53-58.
7. Kulichenko A.Ya., Kuzin M.O., Vakulenko I.O. Otsinka yakisnykh pokaznykiv kontaktuvannia poverkhnevnykh shariv trybolohichnoi systemy «koleso – reika» [Evaluation of quality indicators contacting the surface of the tribological system «wheel – rail»]. *Nauka ta prohres transportu. Visnyk Dnipropetrovskoho natsionalnoho universytetu zaliznychnoho transportu – Science and Transport Progress. Bulletin of Dnipropetrovsk National University of Railway Transport*, 2013, no. 3 (45), pp. 44-52. doi: org/10.15802/stp2013/14529.
8. Muravyev V.V., Noyeva M.R., Sharko A.V. Issledovaniye protsessa raspada peresyschennogo tverdogo rastvora v aluminiiyevom splave D16 [Study of the process of decomposition of the supersaturated solid solution in the aluminum alloy D16]. *Fizika metallov i metallovedeniye – Physics of Metals and Metallography*, 1978, vol. 46, no. 4, pp. 746-749.
9. Lage Y., Cachão H., Reis L. A damage parameter for HCF and VHCF based on hysteretic damping. *Intern. Journal of Fatigue*, 2014, vol. 62, pp. 2-9. doi: 10.1016/j.ijfatigue.2013.10.010.
10. Weigang M., Tingting M., Zhang X. Comprehensive Study of Thermal Transport and Coherent Acoustic-Phonon Wave Propagation in Thin Metal Film–Substrate by Applying Picosecond Laser Pump–Probe Method. *Journal of Physical Chemistry*, 2015, no. 119 (9), pp. 5152-5159. doi: 10.1021/jp512735k.
11. Langman R.A., Mutton P.J. Estimation of Residual Stresses in Railway Wheels by Means of Stress Induced Magnetic Anisotropy. *NDT&E Intern*, 1993, vol. 26, no. 4, pp. 195-205. doi: 10.1016/0963-8695(93)90474-9.
12. Packo P., Bielak T., Spencer A.B. Numerical simulations of elastic wave propagation using graphical processing units–Comparative study of high-performance computing capabilities. *Computer Methods in Applied Mechanics and Engineering*, 2015, vol. 290, pp. 98-126. doi:10.1016/j.cma.2015.03.002.
13. Fukuoka H., Higaro M., Yamasaki T. Ultra-sonic Resonance Method with EMAT for Stress Measurement in Thin Plates. *Review of Progress in Quantitative Nondestructive Evaluation*, 1993, no. 12, pp. 2129-2136. doi: 10.1007/978-1-4615-2848-7_273.
14. Herzer R., Frotscher H., Schillo K. Ultra-sonic Set-Up to Characterize Stress States in Rims of Railroad Wheels. *Nondestructive Characterization of Materials VI*, 1994, pp. 699-706. doi: 10.1007/978-1-4615-2574-5_89.
15. Vakulenko I.A., Proydak S.V. The Influence Mechanism of Ferrite Grain Size on Strength Stress at the Fatigue of Low-carbon Steel. *Nauka ta prohres transportu. Visnyk Dnipropetrovskoho natsionalnoho universytetu zaliznychnoho transportu – Science and Transport Progress. Bulletin of Dnipropetrovsk National University of Railway Transport*, 2014, no. 1 (49), pp. 97-104. doi: 10.15802/stp2014/22668.

PhD, Acc. Prof. S. V. Proydak (Ukraine); PhD, Acc. Prof. O. O. Chaikovskiy (Ukraine) recommended this article to be published

Accessed: Feb. 20, 2015

Received: May 08, 2015